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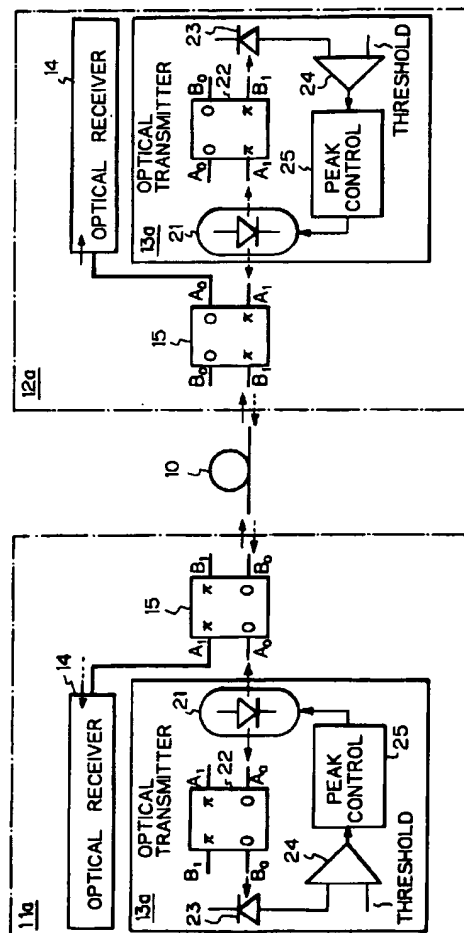
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(54) **Wavelength division multiplex bidirectional optical communication system.**

(57) Bothway optical communication is carried out through wavelength division multiplex system between two terminal stations (11a, 12a), each having a two-beam interference type filter (15) coupled with an optical cable (10) for multiplexing and/or de-multiplexing transmit light and receive light. The filter (15) has pass bands and attenuation bands periodically for wavelength in the communication wavelength band. Wavelength of transmit light is essentially the same as wavelength of receive light in each terminal station, with small offset of two wavelengths less than 5 nm. Oscillation wavelength of the laser (21) for transmission is adjusted so that it coincides with pass band of the filter, which doubles as reference wavelength of oscillation wavelength of the laser. Preferably, said two-beam interference type filter (15) is a Mach Zehnder type asymmetrical interferometer having a pair of directional couplers ((F1, F2) connected to each other through a pair of optical fibers (f1, f2) so that the period of pass bands and/or attenuation bands of the filter (15) is adjustable.

**Fig. 3**



The present invention relates to a bothway wavelength division multiplex optical communication system, in particular, relates to such a system in which wavelengths of lights in two directions belong to single wavelength band, although those wavelengths differ or offset from each other a little in said band, and said wavelengths are finely controlled based upon a single wavelength standard through self tuning operation. The present invention is for instance used for subscriber lines in which large number of cables are necessary used and therefore the use of a single optical cable for bothway communication is essential.

Conventionally, a time compression multiplex (TCM) optical communication system has been used for bothway communication system using a single optical line. In that system, upward direction signal and downward direction signal are forwarded to an optical cable alternately, so, that system has been used for low rate communication up to 28 Mb/s/second.

When high rate communication is requested in a system with a single optical cable, for instance, it is higher than 50 Mb/s/second, a wavelength division multiplex (WDM) optical communication system has been used. That system uses two wavelength bands, for instance 1.3  $\mu\text{m}$  band and 1.5  $\mu\text{m}$  band for upward direction and downward direction, respectively.

Fig. 1A shows a block diagram of a prior bothway wavelength division multiplex (WDM) optical communication system. In the figure, the numeral 70 is a single optical fiber cable coupling a pair of terminal stations 71 and 72, each having an optical transmitter 73 which outputs light signal through a laser, an optical receiver 74 which receives optical signal from an opposite side, and a multiplexer/demultiplexer 75 having an output port coupled with the single optical fiber cable 70 and a pair of input ports coupled with the transmitter 73 and the receiver 74 so that the light from the transmitter 73 is forwarded to the optical cable 70 and the light from the line 70 is forwarded to the receiver 74. The wavelength of output of the transmitter 73 differs from that in another side, for instance, wavelength in one direction is 1.3  $\mu\text{m}$  band, and wavelength in the other direction is 1.5  $\mu\text{m}$  band. Those lights of 1.3  $\mu\text{m}$  band and 1.5  $\mu\text{m}$  band are multiplexed in the optical cable 70.

However, the system of Fig. 1A has the disadvantage that a laser in a transmitter 73 must provide oscillation wavelength which coincides with center of pass band of a multiplexer/demultiplexer. However, it should be noted that oscillation wavelength of a laser depends upon ambient temperature, bias current and/or producing error, and therefore, it is rather difficult to obtain a laser with requested accurate oscillation wavelength. Further, the difference between wavelengths in two directions must be large enough for suppressing cross talk between two wavelengths,

and therefore, two kinds of lasers through different producing processes must be used for large oscillation wavelength difference, for instance, 1.3  $\mu\text{m}$  and 1.5  $\mu\text{m}$ . Therefore, producing yield rate of a laser is rather low, and so, the cost of the communication system of Fig. 1A is rather high.

Fig. 1B shows another bothway wavelength division multiplex optical communication system, which uses the common single wavelength band in both directions. The system of Fig. 1B has not existed in a market, but we considered it in our research. In the figure, the numeral 80 is an optical cable having a pair of ends each coupled with terminal stations 81 and 82. Each of the terminal stations has an optical transmitter 83, an optical receiver 84 for receiving light from the other side, and a directional coupler 85 coupled with an end of the optical cable 80, an output of the optical transmitter 83, and an input of the optical receiver 84, so that the light from the transmitter 83 is applied to the optical cable 80, and the light from the optical cable 80 is applied to the optical receiver 84.

However, the system in Fig. 1B has the disadvantage that the receiver 84 receives not only the light from the optical cable 80 but also the light from the transmitter 83 in the same terminal station through the leakage in the directional coupler 85, and therefore, the signal characteristics are deteriorated, although the lasers in the transmitters in each stations oscillate with the same wavelength as each other.

In accordance with the present invention, a wavelength division multiplex bothway optical communication system comprises a first terminal station, and a second terminal station coupled with said first terminal station through an optical communication pathway, wherein each terminal station comprises a transmitter having a laser for converting a transmission electrical signal to an optical signal, an optical receiver for receiving an optical signal which is to be subsequently converted to an electrical signal, and a two-beam interference type first filter having a zero phase input port and a pi phase input port coupled with an output of the laser and an input of said optical receiver, respectively, and a zero phase output port and a pi phase output port with one output port being coupled with the optical communication pathway and the other port being free standing, the optical communication pathway being coupled with the zero phase output port of one terminal station and the pi phase output port of the other terminal station, wherein the filter has a periodic characteristic of pass band and attenuation band for wavelengths in a communication wavelength band, wherein each terminal station has wavelength control means for controlling oscillation wavelength of said laser so that said oscillation wavelength coincides with the centre of the pass band of said filter, wherein the wavelength control means comprises monitor means for monitoring the output

wavelength of the laser, a comparator for comparing the strength of the monitored output with a predetermined threshold level and to provide a corresponding output, and control means for adjusting the oscillation wavelength of the laser based upon the output of the comparator so that the oscillation wavelength substantially coincides with the pass band of the filter, and wherein the wavelength band of the laser in the first terminal station is essentially the same as the wavelength band of the laser in the second terminal station and is in communication wavelength band.

The present invention overcomes the disadvantages and limitations of the prior bothway wavelength division multiplex optical communication system by providing a new and improved bothway wavelength multiplex optical communication system.

The present invention provides a bothway wavelength division multiplex optical communication system which uses essentially a common wavelength band in both directions.

The present invention also enables a filter for separating receiving wavelength from transmitting wavelength to double as a wavelength standard for a laser in a transmitter.

In one example of a bothway wavelength division multiplex communication system is provided in which two terminal stations have a master-slave relationship, and the filter for directional coupling in the master station provides wavelength standard for a laser in a transmitter in the master station, a filter for directional coupling in the slave station, and a laser for a transmitter in the slave station.

Some examples of communication systems according to the invention together with some prior configurations are illustrated in the accompanying drawings, in which:-

Fig.1A shows a prior bothway optical communication system using two wavelengths;

Fig.1b shows another prior bothway optical communication system using single wavelength;

Fig.2 shows explanatory figures of a two-beam interference type filter;

Fig.3 is a block diagram of an embodiment of a bothway wavelength division multiplex optical communication system according to the present invention;

Fig.4A is a block diagram of another embodiment of the bothway wavelength division multiplex optical communication system according to the present invention,

Fig.4B is a block diagram of still another embodiment of the bothway wavelength division multiplex optical communication system according to the present invention,

Fig.4C is a block diagram of still another embodiment of the bothway wavelength division multiplex optical communication system according to the present invention,

Fig.5 is a block diagram of still another embodiment of the bothway wavelength division multiplex optical communication system according to the present invention,

Fig.6 is a block diagram of still another embodiment of the bothway wavelength division multiplex optical communication system according to the present invention,

Fig.7 shows experimental curves showing relations between period of pass bands or attenuation bands of the two beam interference type filter, and period of oscillation wavelengths of the laser according to the present invention.

Some of the important features of the present invention are that the use of a two-beam interference type filter as a multiplexer/de-multiplexer in wavelength division multiplex communication system, and that said two-beam interference type filter doubles as wavelength standard for determining oscillation wavelength of a laser in a transmitter.

First, a two-beam interference type filter is described in accordance with Fig.2.

Fig.2A shows structure of a two-beam interference type directional coupler, having a pair of optical fibers C1 and C2 which are optically coupled with each other in the region F in a predetermined length so that the optical fibers C1 and C2 have common clad layer in that region F. The coupler has a pair of input ports C1-1 and C2-1, and a pair of output ports C1-2 and C2-2. As the directional coupler is reversible, the input ports and the output ports may be reversed. Each of input ports and each of output ports are called a zero phase port and a pi phase port.

In operation of said directional coupler, when input light is applied to one of the input ports, the input light is divided to two output ports so that each output port outputs optical power having the level of -3B as compared with the input optical power. So, the directional coupler of Fig.2A is called a 3 dB coupler.

When the coupling region F is designed properly, the ratio of the output optical power to each output ports depends upon wavelength of input light. So, it functions as a wavelength filter.

When it operates as a wavelength filter, assuming that input light is applied to the zero phase port C1-1, it is switched to the output port C1-2 or the output port C2-2, depending upon wavelength of the input light. Similarly, input light to the pi phase port C2-1 is switched to the output port C1-2 and the output port C2-2, depending upon wavelength of the input light.

The transmission factor, and/or the attenuation factor of the filter has periodic characteristics as shown in Fig.2B, where horizontal axis shows wavelength of input light, and vertical axis shows strength of output light when input light is applied to the zero phase input port C1-1. The solid curve (a) shows the output at the zero phase output port C1-2, and the

dotted curve (b) shows the output at the pi phase output port C2-2.

Threshold level  $L_1$  and/or  $L_2$  is defined for self tuning purposes of a laser as described later. The higher threshold level  $L_1$  is the same as the peak output of the filter, or a little lower than the peak output. The lower threshold level  $L_2$  is almost zero or a little higher than zero.

In practical use, a pair of directional couplers F1 and F2 of Fig.2A are coupled through a pair of optical fibers f1 and f2 as shown in Fig.2C. The symbol F1 or F2 shows a directional coupler in Fig.2A. The zero phase port of the first directional coupler F1 is coupled with the zero phase port of the second directional coupler F2 through the optical fiber f1, and the pi phase port of the first directional coupler F1 is coupled with the pi phase port of the second directional coupler F2 through the optical fiber f2. The optical length of the fibers or the optical wave-guides f1 and f2 differs by  $\Delta L$ . We call the structure of Fig.2C an asymmetrical Mach Zehnder type filter, or an asymmetrical Mach Zehnder type interferometer.

The advantage of the structure of Fig.2C is that the period ( $=2 \times \text{FSR}$ ; Free Spectrum range) between the wavelength for the peak of the pass band and the peak of the attenuation band may be adjusted by adjusting the difference  $\Delta L$  of the length of the fibers f1 and f2.

The frequency band  $\Delta F$  from the frequency for the peak output to the frequency for the minimum output of the filter in Fig.2C is shown below.

$$\Delta F = c / (2 \times n_{\text{eff}} \times \Delta L)$$

where  $c$  is light velocity,  $n_{\text{eff}}$  is effective refractive index of a waveguide or a fiber, and  $\Delta L$  is difference of length of optical fibers f1 and f2 coupling directional couplers F1 and F2. A Mach Zehnder type filter having  $\Delta F$  up to 640 GHz is possible to produce.

Fig.2D shows the modification of an asymmetrical Mach Zehnder type filter, which has a heater H on one of the intermediate optical fibers f1 and f2. The heater H is heated by the power source P. The structure of Fig.2D has the advantage that the period (FSR or  $\Delta F$ ) or the tuning wavelength is controlled finely by controlling temperature of the heater H. The value FSR is increased around 0.5-1.0 nm for each temperature when temperature is increased. That is described in The Institute of Electronics, Information and Communication Engineer in Japan, Trans. Commun., vol. E75-B, No.9, September 1992, pages 871-879.

A Mach Zehnder type filter may be produced on a quartz waveguide. When the period FSR is the wider, the size of the filter is the smaller, the producing error is the smaller, and the transmission characteristics of the filter may be uniform.

A port of the filter may have a spherical tapered end so that it is well coupled with an optical fiber optically.

The two-beam interference type directional cou-

pler or a filter of Figs.2A through 2D is described in Journal of lightwave technology, vol 6, No.6, June 1988, pages 1003-1010.

Fig.3 shows a block diagram of an embodiment of a wavelength division multiplex bothway optical communication system according to the present invention. In the figure, a pair of terminal stations 11a and 12a are coupled through an optical cable 10. Each of the terminal stations 11a and 12a has an optical transmitter 13a, an optical receiver 14, and a filter 15 which operates to multiplex/de-multiplex transmit light and receive light.

The filter 15 is a two-beams interference type filter of Fig.2A, or an asymmetrical Mach Zehnder type interferometer as shown in Fig.2C and Fig.2D. In case of Fig.2C or Fig.2D, the period of pass bands of the filter is adjustable.

The filter 15 has the transmission characteristics as shown in Fig.2B, where solid line shows transmission characteristics when input light is applied to zero phase input port, and output light is at zero phase output port. Dotted line shows transmission characteristics when input light is applied to pi phase port, and output light is at zero phase output port. The dotted line is the same as the transmission characteristics at pi phase output port when input light is applied to zero phase input port.

The filter 15 is reversible. So, input ports and output ports may be reversed. But, we refer to input ports and output ports for the sake of simplicity of explanation.

It is assumed that input ports have zero phase port  $A_0$  and pi phase port  $A_1$ , and output ports have zero phase port  $B_0$  and pi phase port  $B_1$ .

The optical cable 10 is coupled with the outputs of the filters 15 so that the transmission characteristics of the output port of the first terminal station differs from that of the second terminal station. In the embodiment, the cable 10 is coupled with the port  $B_0$  (zero phase) in the station 11a, and the port  $B_1$  (pi phase) in the station 12a.

The optical receiver 14 is coupled with the filter 15 in the port which has the same transmission characteristics as that of the output port in the opposite station. In the embodiment, the optical receiver 14 in the station 11a is coupled with the input port  $A_1$  (pi phase), (the output port of the opposite station 12a is  $B_1$  (pi phase), and the optical receiver 14 in the station 12a is coupled with the input port  $A_0$  (zero phase), where the output port of the opposite station 11a is  $B_0$  (zero phase).

The optical transmitter 13a is coupled with the filter 15 in the input port having the same transmission characteristics as the output port which is coupled with the optical cable 10. In the embodiment, the optical transmitter 13a in the station 11a is coupled with the input port  $A_0$  (zero phase), where the optical cable 10 is coupled with the output port  $B_0$  (zero phase), and

the optical transmitter 13a in the station 12a is coupled with the input port  $A_1$  (pi phase) where the optical cable 10 is coupled with the output port  $B_1$  (pi phase).

The light from the transmitter 13a in the station 11a is forwarded, through the port  $A_0$  (zero phase) of the filter 15 in the station 11a, the output port  $B_0$  of the filter, the optical cable 10, the output port  $B_1$  (pi phase) of the filter 15 in the station 12a, and the input port  $A_0$  (zero phase) of the filter 15 in the station 12a, to the optical receiver 14 in the station 12a. Similarly, the light from the transmitter 13a in the station 12a is forwarded, through the port  $A_1$  (pi phase) of the filter 15 of the station 12a, the port  $B_1$  (pi phase) of the filter 15 in the station 12a, the optical cable 10, the port  $B_0$  of the filter 15 in the station 11a, and the port  $A_1$  in the filter in the station 11a, to the optical receiver 14 in the station 11a.

Therefore, it should be noted that the ports of the filter are used in opposite manner (opposite phase) in the corresponding means in each stations.

It should be appreciated that wavelength band from the first station 11a is in the same wavelength band as that from the second station 12a. It is for instance 1.3  $\mu\text{m}$  band, or 1.5  $\mu\text{m}$  band. The wavelength from the first station 11a differs a little from the wavelength from the second station 12a in the same wavelength band. The difference or offset between two wavelengths is for instance less than 5 nm. Thus, two wavelengths are multiplexed in an optical cable 10, and bothway communication is carried out by using a single optical cable.

Next, the self tuning of a laser so that oscillation wavelength of a laser 21 coincides with center of pass band of a filter 15 is described. In the embodiment, a second filter 22 for self tuning purposes is provided in each stations 11a and 12a for defining reference wavelength. The second filter 22 is also a two-beam interference type filter, or asymmetrical Mach Zehnder type interferometer, having the same pass band characteristics as that of the first filter 15. The second filter 22 has input ports  $A_0$  (zero phase) and  $A_1$  (pi phase), and output ports  $B_0$  (zero phase) and  $B_1$  (pi phase).

A semiconductor laser provides front light and back light in opposite direction. Front light is used for transmitting signal to another station, and back light is used for self tuning of wavelength of the laser.

Back light of the laser 21 is applied to one of the input ports of the tuning filter 22, which provides output light to an optical-electrical converter or sensor 23 through an output port having the same transmission characteristics as that of the output port of the filter 15. In the embodiment of Fig.3, back light of the laser 21 in the station 11a is applied to the port  $A_0$  (zero phase) of the filter 22, and the output of the port  $B_0$  (zero phase) is applied to the converter 23. Similarly, back light in the station 12a is applied to the port  $A_1$  (pi phase) of the filter 22, and the output of the port

$B_1$  (pi phase) is applied to the converter 23.

The output of the converter 23 is applied to the comparator 24, which compares the output of the converter 23 with a predetermined threshold level  $L_1$  (Fig.2B), which is close to the maximum level of the transmission power but a little lower than the same. The comparator 24 provides positive output only when the output of the converter 23 exceeds the threshold level. The peak control 25 receives the output of the comparator 24, and controls the oscillation wavelength of the laser 21 so that output of the reference filter 22 is the maximum. The manner for adjusting oscillation wavelength of a laser is conventional, and it is possible by adjusting temperature of a laser, and/or bias current of a laser.

Two terminal stations 11a and 12a have the above closed feed back loop for controlling oscillation wavelength. The station 11a receives back light of the laser 21 at the zero phase input port  $A_0$  of the filter 22 which outputs the light at the zero phase output port  $B_0$  and the peak control 25 controls so that the oscillation wavelength of the laser 21 coincides with pass band of the filter 22, so that the output of the filter 22 is the maximum. Thus, the oscillation wavelength of the laser 21 is controlled so that it coincides with the wavelength which provides the peak or the maximum transmission of the filter 22 for zero phase.

Similarly, the oscillation wavelength of the laser 21 in the station 12a is controlled so that it coincides with the wavelength which provides the peak or the maximum transmission of the filter 22 for pi phase.

Therefore, the wavelength band of two stations is in the same wavelength band, and the wavelength of a first station is offset or shifted by the pi phase from that of a second station.

The combination of the reference filter 22, the sensor 23, the comparator 24, and the control 25 constitute a monitor means for monitoring and controlling oscillation wavelength of the laser 21.

The two-beam interference type filter 15 has the features that the insertion loss is small, and the leakage of transmit light to an optical receiver is small.

The filter 15 has the periodical characteristics as shown in Fig.2B. Therefore, it is only necessary to coincide oscillation wavelength of a laser with one of the transmission wavelengths of the filter.

Further, it is easy and simple in the present invention to coincide transmission wavelength of a filter in a receive side with that of a transmit side.

Further, the requested value of adjustment of oscillation wavelength of a laser is small, and the use of a pair of lasers having oscillation wavelength in the same band is possible in both the end terminals. It should be noted that a laser in a prior art of Fig.1A must be adjusted in wide range so that oscillation wavelength coincides with pass band of a filter, and further, lasers of different oscillation wavelengths are requested in two terminal stations.

In one modification, a peak control 25 may operate so that output of an optical-electrical converter 23 becomes the maximum so that transmission optical power into the cable 10 is the maximum, although the embodiment of Fig.3 has the comparator 24 to compare the output of the converter 23 with the predetermined threshold.

In another modification, a two-beams interference type filter may be substituted with another filter which has periodical and complementary characteristics shown in Fig.2B, for instance, a ring resonator, and a Fabry-Perot Etalon filter, although the former has too high Q, which would cause the operation unstable, and are difficult to have long period, and the latter is difficult to adjust an optical coupling axis, which can not unify the periodical characteristics between each filters.

Figs.4A, 4B and 4C show modifications of the embodiment of Fig.3 of the present invention. The features of those modifications reside in the structure for controlling oscillation wavelength of a laser to coincide with pass band of a filter 15. In those modifications, only one end terminal is shown for the sake of simplicity.

In Fig.4A, the terminal station 11b has an optical transmitter 13b, an optical receiver 14, and a filter 15 which is optically coupled with an optical cable 10. The optical transmitter 13b has a laser 21 for oscillating transmission light, a reference wavelength filter 22, an optical-electrical converter 23, a comparator 24, and a bottom control 26. The feature of Fig.4A as compared with the embodiment of Fig.3 is that the reference wavelength filter 22 receives back light of the laser 21 on the pi phase port  $A_1$  when front light of the laser is applied to the zero phase port  $A_0$  of the filter 15. That is to say, back light of the laser is received by the reference wavelength filter 22 on the port which is in different phase from that of the receiving port of the filter 15.

The comparator 24 in this case compares the output of the converter 23 with the threshold which is close to bottom value  $L_2$  in output of the filter (see Fig.2B). The bottom control 26 controls the oscillation wavelength of the laser 21 so that the output of the reference filter 22 is less than the threshold  $L_2$ . Thus, the oscillation wavelength of the laser 21 coincides with the pass band of the filter 22.

Fig.4B shows a block diagram of another modification of the embodiment of Fig.3. The feature of Fig.4B is that the terminal station 11c has no reference wavelength filter, but an asymmetrical branch ratio type directional coupler 31 is provided between an output of a filter 15 and an optical cable 10, so that a small part of transmission optical power is branched to be applied to an optical-electrical converter or a sensor 23. A control 25 in this case is a peak control which controls a laser so that output power of the sensor 23 is higher than a predetermined threshold  $L_1$ .

The filter 15 operates not only for multiplexing and/or de-multiplexing transmit light and receive light, but doubles as a wavelength reference filter.

It should be noted that the filter 15 and the directional coupler 31 are integrated on the common substrate B, by using a quartz waveguide.

Fig.4C shows a block diagram of still another modification of the embodiment of Fig.3. The feature of Fig.4C is that the terminal station 11d has no reference wavelength filter, but the optical-electrical converter 23 receives the light from the free standing output port  $B_1$  of the filter 15 for the purpose of controlling the oscillation wavelength of the laser 21. The control 26 in this case is a bottom control which controls the output of the sensor 23 to be the bottom  $L_2$  or the minimum.

Fig.5 shows a block diagram of wavelength division multiplex bothway optical communication system according to the present invention. The embodiment of Fig.5 is the combination of the present wavelength division multiplex system of Figs.3 through 4C, and the prior art of Fig.1B, and may communicate by using four wavelengths.

In Fig.5, the terminal stations 11e, 11f, 12e and 12f are a terminal station of Fig.3, Fig.4A, Fig.4B or Fig.4C. The terminal stations 11e in one terminal and the terminal station 12e in the other terminal operate for instance in 1.3  $\mu\text{m}$  band, and the terminal stations 11f and 12f operate for instance in 1.5  $\mu\text{m}$ . The wavelengths of 1.3  $\mu\text{m}$  band and 1.5  $\mu\text{m}$  band are multiplexed or de-multiplexed in the multiplexer/demultiplexer 75. Therefore, four wavelengths (two wavelengths in 1.3  $\mu\text{m}$  band, and two wavelengths in 1.5  $\mu\text{m}$  band) are multiplexed in the optical cable 10.

Fig.6 shows a block diagram of the optical communication system, according to the present invention, which functions to coincide the wavelength of a laser and a filter in both the end stations. In Fig.6, one of the end stations operates as a master station, and the other end station operates as a slave station which follows the master station in wavelength of a laser and a filter. In Fig.6, the station (a) operates as a master station, and the station (b) operates as a slave station.

The master station (a) in Fig.6 has the structure of Fig.4C. However, it should be appreciated of course that another structure, for instance, Fig.3, Fig.4A, or Fig.4B may be possible.

The basic idea for coinciding wavelength of a laser and a filter in both the end stations is as follows.

a) A filter for multiplexing/demultiplexing transmit light and receive light in a master station operates to provide reference wavelength.

b) The oscillation wavelength of a laser for providing transmit light in a master station is controlled so that it coincides with pass band of said filter in the master station.

c) The filter for multiplexing/demultiplexing trans-

mit light and receive light in a slave station is then controlled so that the pass band of said filter in the slave station receives the maximum level of light from the master station.

d) The oscillation wavelength of a laser for providing transmit light in the slave station is then controlled so that it coincides with pass band of the filter in the slave station.

Therefore, it should be appreciated that the pass band of the filter in both the stations coincide with each other, and the oscillation wavelength of the lasers in both the stations coincides with said pass band.

In Fig.6, the master station 11d has a filter 15M, which functions as reference of wavelength in communication system. The oscillation wavelength of a laser 21M for providing transmit light in the master station 11d is then controlled so that it coincides with pass band of the filter 15M in the master station 11d, as described in accordance with Fig.4C.

In a slave station, optical light applied to the slave station (Fig.6B) from the optical cable 10 is applied to an optical-electrical converter 23b through the filter 15S. The electrical signal of the output of the converter 23b is then applied to an optical receiver 14 which has a linear amplifier 102 functioning AGC (automatic gain control). The output of the amplifier 102 provides receive signal of the optical communication system. The output of the amplifier 102 is also applied to a thermal control circuit 101 which supplies a heater H in the filter 15S the power so that the pass band of the filter 15S is shifted according to the power thus applied so that the output of the amplifier 102 has the maximum level. Thus, the center of the pass band of the filter 15S which has a pair of directional couplers F1 and F2 coupled with each other through a pair of asymmetrical optical fibers one of which has a heater H is controlled so that it coincides with the wavelength of receive light.

Then, oscillation wavelength of the laser 21S for providing transmit light is controlled so that it coincides with pass band of the filter 15S, through the feed back loop having the filter 15S, the optical-electrical converter 23a, the comparator 24 which receives threshold level for comparison, and the bottom control circuit 26. The operation of the feed back loop has been described in accordance with Fig.4C. It should be appreciated of course that the feed back loop for controlling oscillation wavelength of the laser 21S is not limited to that of Fig.4C, but another circuit of Fig.3, Fig.4A or Fig.4B is possible.

In practical embodiment, it is preferable that the time constant in the feed back loop for controlling the pass band of the filter 15S, including the heater H, and the thermal control circuit 101, is shorter than the time constant in the feed back loop for controlling the oscillation wavelength of the laser 21, including the comparator 24 and the bottom control 26.

Next, the period of the pass band (FSR) of a filter,

and the period of longitudinal modes of a laser are discussed.

It is well known that there are two kinds of lasers, a multi-longitudinal mode oscillation laser (for instance a Fabry-Perot laser), and a single-longitudinal mode oscillation laser (distributed feed back laser, or distributed Bragg Reflection laser).

A multi-longitudinal mode oscillation laser satisfies the following equation.

$$q \times (\lambda)/(2n) = L$$

where  $(\lambda)$  is oscillation wavelength in vacuum,

L is length of a resonator of a laser,

n is refractive index of medium,

q is number of standing waves of half wavelength in the resonator.

As L is much larger than wavelength  $(\lambda)$ , many waves having different wavelength from each other are generated in the laser, and the oscillation wavelength of the laser is determined so that the gain is the maximum in said many waves. For instance, a laser of 1.3  $\mu\text{m}$  has the period of longitudinal modes of 0.8 nm (determined by n and L in above equation).

Therefore, it is preferable that the period ( $=2 \times \text{FSR}$ ) of the pass bands of a filter coincides with the period of longitudinal modes of a laser so that output power of the laser is transmitted to a receiver with high efficiency, and even when transmit light of a laser is reflected by a connector at an end of an optical cable, it would be prevented by the filter with no affection of side modes of a signal light, so that the deterioration of an optical receiver due to reflected back light is solved.

When a laser is a single-longitudinal mode oscillation laser, no consideration about said periods is necessary.

Fig.7 shows experimental curves of side modes in back light where horizontal axis shows difference of center wavelength of pass band of a filter, and center oscillation wavelength of a laser in nm, and vertical axis shows attenuation (dB) in back light through the filter as compared with front light.

The curve (a) in Fig.7 shows the case that the period of the pass bands of a filter coincides with the period of the longitudinal modes of a laser, and  $\text{FSR}=0.8 \text{ nm}$ . It should be appreciated in the curve (a) that the attenuation of back light is 30 dB when the center wavelength of pass band of the filter coincides with the center oscillation wavelength of the laser, and said attenuation is 16 dB when the difference of wavelengths is 0.6 nm.

On the other hand, the curve (b) shows the case that the period of the filter does not coincide with the period of the laser, where  $\text{FSR}=5 \text{ nm}$ . In that case, the attenuation of back light is around 10 - 12 dB for each difference of the wavelengths of the laser and the filter.

The requested value of attenuation of back light as compared with desired front light is generally 12

dB. Therefore, the curve (a) in which the period of the pass band of a filter coincides with the longitudinal modes of a filter is satisfactory in practice.

From the foregoing it will now be apparent that a new and improved wavelength division multiplex bothway optical communication system has been found.

## Claims

1. A wavelength division multiplex bothway optical communication system comprising a first terminal station (11a), and a second terminal station (12a) coupled with said first terminal station through an optical communication pathway (10), wherein each terminal station comprises a transmitter (13a) having a laser (21) for converting a transmission electrical signal to an optical signal, an optical receiver (14) for receiving an optical signal which is to be subsequently converted to an electrical signal, and a two-beam interference type first filter (15) having a zero phase input port ( $A_0$ ) and a pi phase input port ( $A_1$ ) coupled with an output of the laser (21) and an input of said optical receiver (14), respectively, and a zero phase output port ( $B_0$ ) and a pi phase output port ( $B_1$ ) with one output port being coupled with the optical communication pathway (10) and the other port being free standing, the optical communication pathway being coupled with the zero phase output port of one terminal station (11a) and the pi phase output port of the other terminal station (12a), wherein the filter (15) has a periodic characteristic of pass band and attenuation band for wavelengths in a communication wavelength band, wherein each terminal station (11a, 12a) has wavelength control means for controlling oscillation wavelength of said laser (21) so that said oscillation wavelength coincides with the centre of the pass band of said filter (15), wherein the wavelength control means comprises monitor means for monitoring the output wavelength of the laser (21), a comparator (24) for comparing the strength of the monitored output with a predetermined threshold level and to provide a corresponding output, and control means (25) for adjusting the oscillation wavelength of the laser (21) based upon the output of the comparator so that the oscillation wavelength substantially coincides with the pass band of the filter (15), and wherein the wavelength band of the laser (21) in the first terminal station (11a) is essentially the same as the wavelength band of the laser (21) in the second terminal station (12a) and is in the communication wavelength band.
2. A wavelength division multiplex bothway optical

communication system according to claim 1, wherein said monitor means has another two-beam interference type filter (22) having similar characteristics to those of the first filter (15), for receiving back light from the laser (21) to the same phase input port ( $A_0$ ) as that of the first filter ( $A_0$ ), and a sensor (23) for converting optical signals of the back light through the second filter (22) to electrical signals, wherein the control means (25) adjusts the oscillation wavelength of the laser (21) so that the output of the second filter (22) is a maximum.

3. A wavelength division multiplex bothway optical communication system according to claim 1, wherein said monitor means has another two-beam interference type filter (22) having similar characteristics to those of the first filter (15) for receiving back light from the laser to the complementary phase input port ( $A_1$ ) to that of the first filter ( $A_0$ ), and a sensor (23) for converting optical signals of the back light through the second filter (23) to electrical signals, wherein the control means (26) adjusts the oscillation wavelength of the laser (21) so that the output of the second filter (22) is a minimum.
4. A wavelength division multiplex bothway optical communication system according to claim 1, wherein the monitor means has a directional coupler (31) downstream of the first filter (15) to branch a part of the output of the laser (21), a sensor (23) for converting optical signals output from the coupler to electrical signals, a comparator (24) for comparing the output of the sensor (23) with a predetermined threshold level, and control means (25) for controlling the oscillation wavelength of the laser so that the output of the sensor is a maximum.
5. A wavelength division multiplex bothway optical communication system according to claim 1, wherein the monitor means has a sensor (23) for receiving optical light from a free standing output port of the first filter (15) which is not coupled with the optical pathway to convert the optical light to electrical signals, a comparator (24) for comparing the output of the sensor (23) with a predetermined threshold level, and control means (26) for controlling the oscillation wavelength of the laser (21) so that light at the free standing port of the first filter (15) is a minimum.
6. A wavelength division multiplex bothway optical communication system according to any of claims 1 to 5, wherein the two-beam interference type filter is a Mach-Zehnder type asymmetrical interferometer having a pair of directional cou-



plers coupled with each other through a pair of optical waveguides having different lengths to each other, and tuning wavelength control means for controlling the optical tuning wavelength of pass band of the filter by adjusting the temperature of at least a part of one of said pair of optical fibres.

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7. A wavelength division multiplex bothway optical communication system according to claim 6, wherein the filter in the first terminal station operates as standard of wavelength for communication, the wavelength of the laser in the first terminal station is controlled so that the oscillation wavelength of the laser coincides with pass band of said filter, the filter in the second terminal station is controlled so that light received from the first terminal station is a maximum by adjusting the temperature of one of the optical fibres coupling the directional couplers, and the oscillation wavelength of the laser in the second terminal station is controlled so that it coincides with the pass band of the filter in the second terminal station.

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8. A wavelength division multiplex bothway optical communication system according to any of the preceding claims, wherein the or each laser (21) is a multi-mode longitudinal mode type laser and wherein the period of the longitudinal mode coincides with the period of pass band of the first filter (15).

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9. A wavelength division multiplex bothway optical communication system according to any of the preceding claims, wherein the communication band is 1.3  $\mu\text{m}$ .

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10. A wavelength division multiplex bothway optical communication system according to any of claims 1 to 8, wherein said communication band is 1.5  $\mu\text{m}$ .

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11. A wavelength division multiplex bothway optical communication system according to any of the preceding claims, wherein the communication pathway is defined by an optical cable.

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Fig. 1A

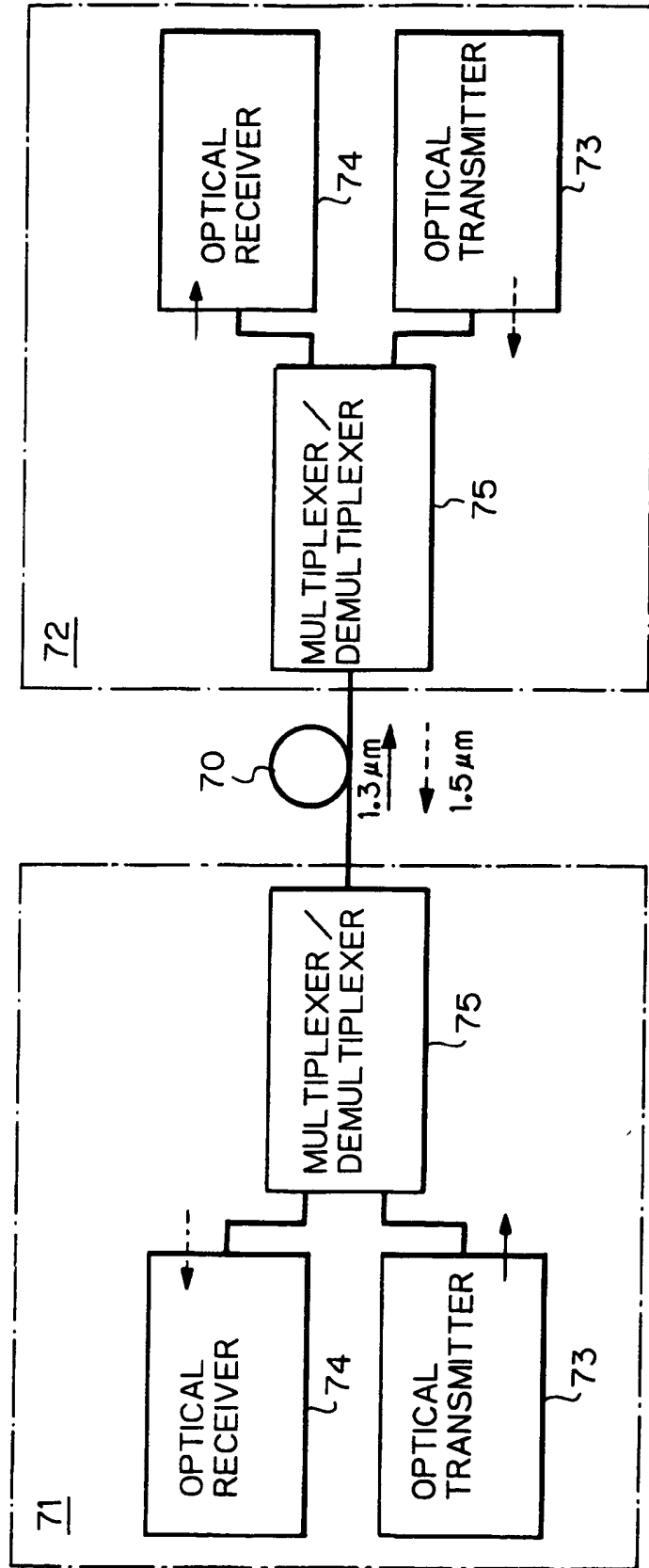
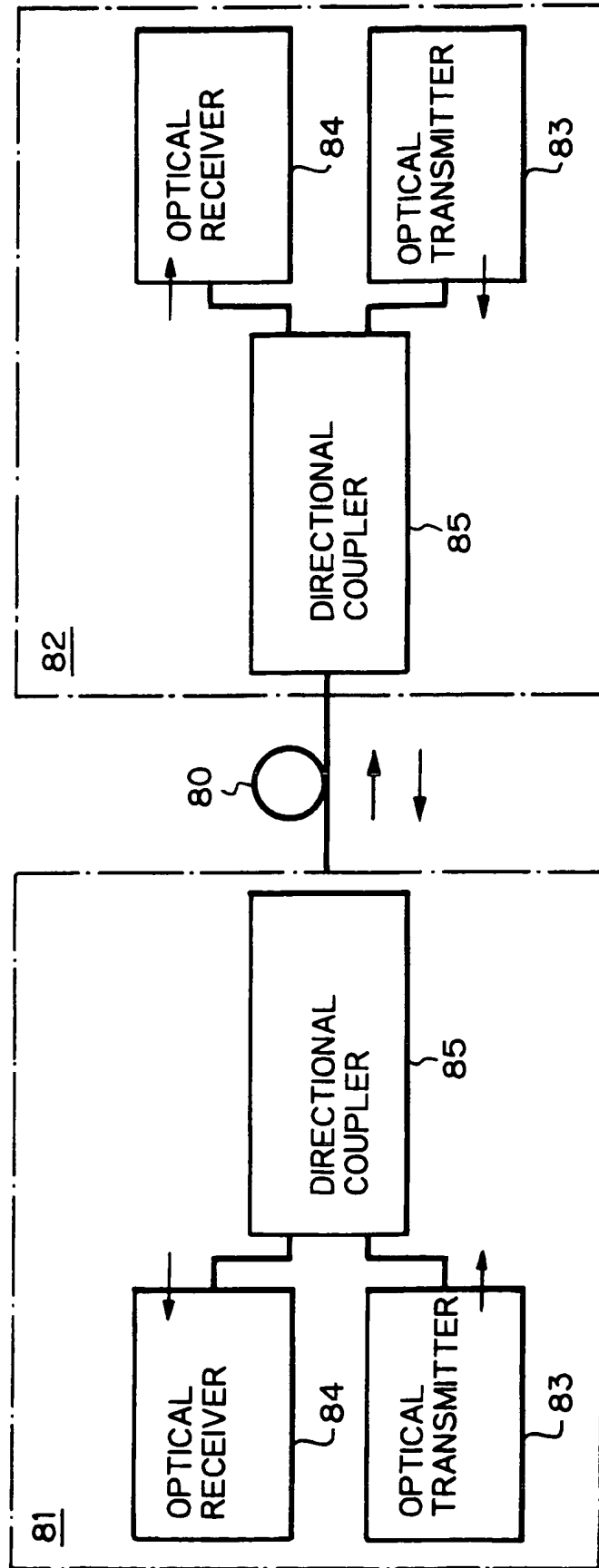


Fig. 1B



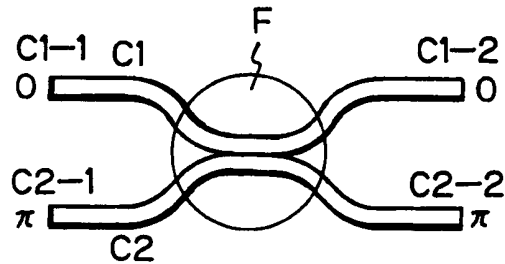
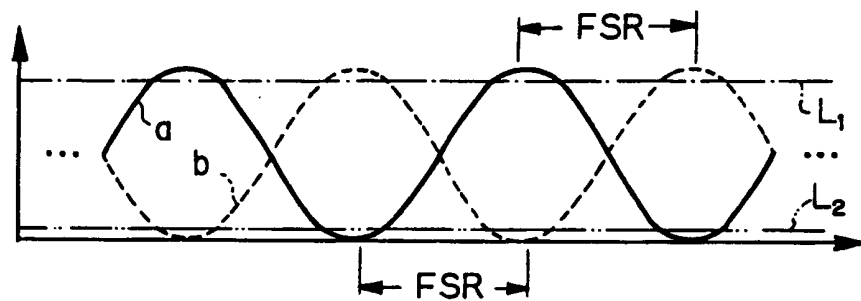
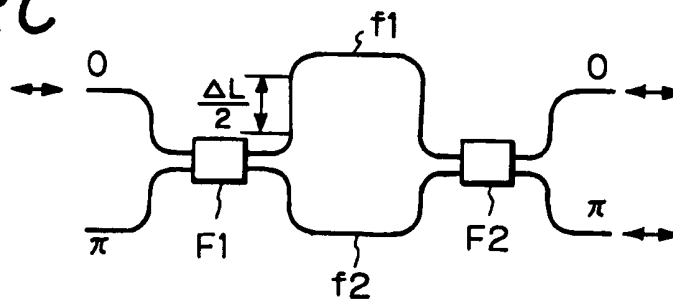
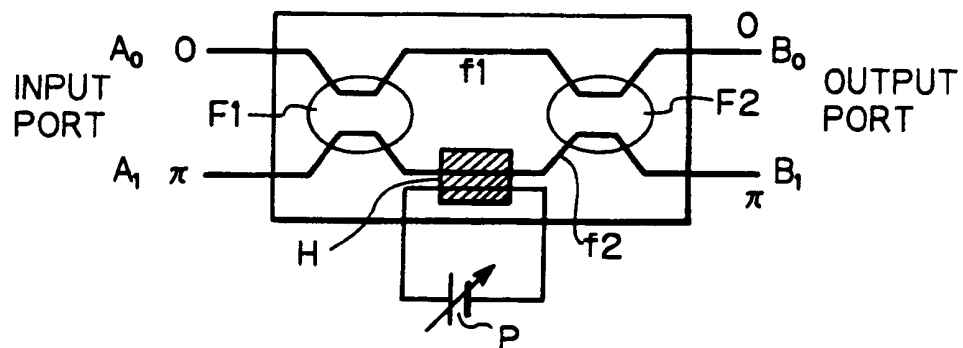
*Fig. 2A**Fig. 2B**Fig. 2C**Fig. 2D*

Fig. 3

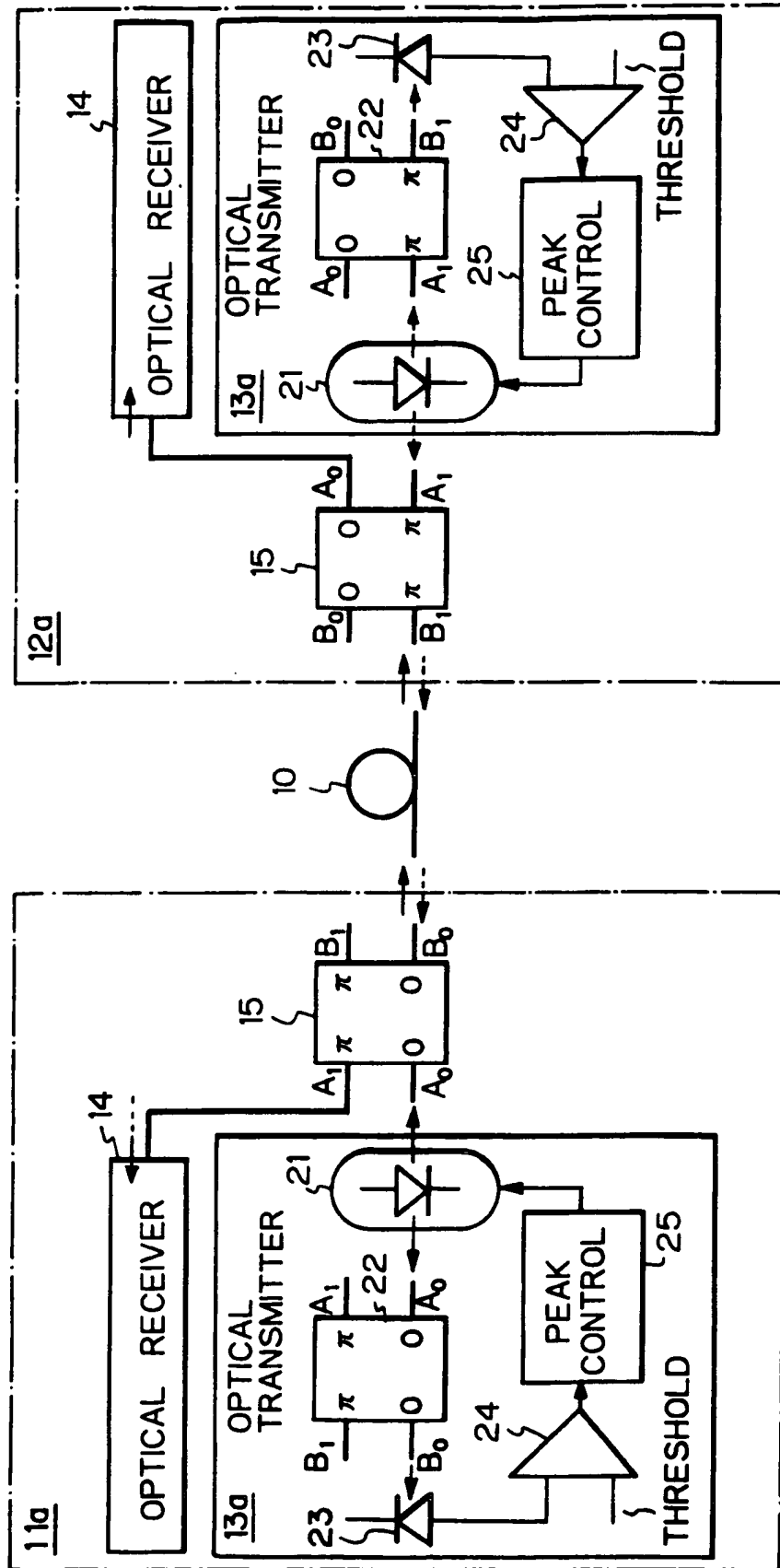




Fig. 4B

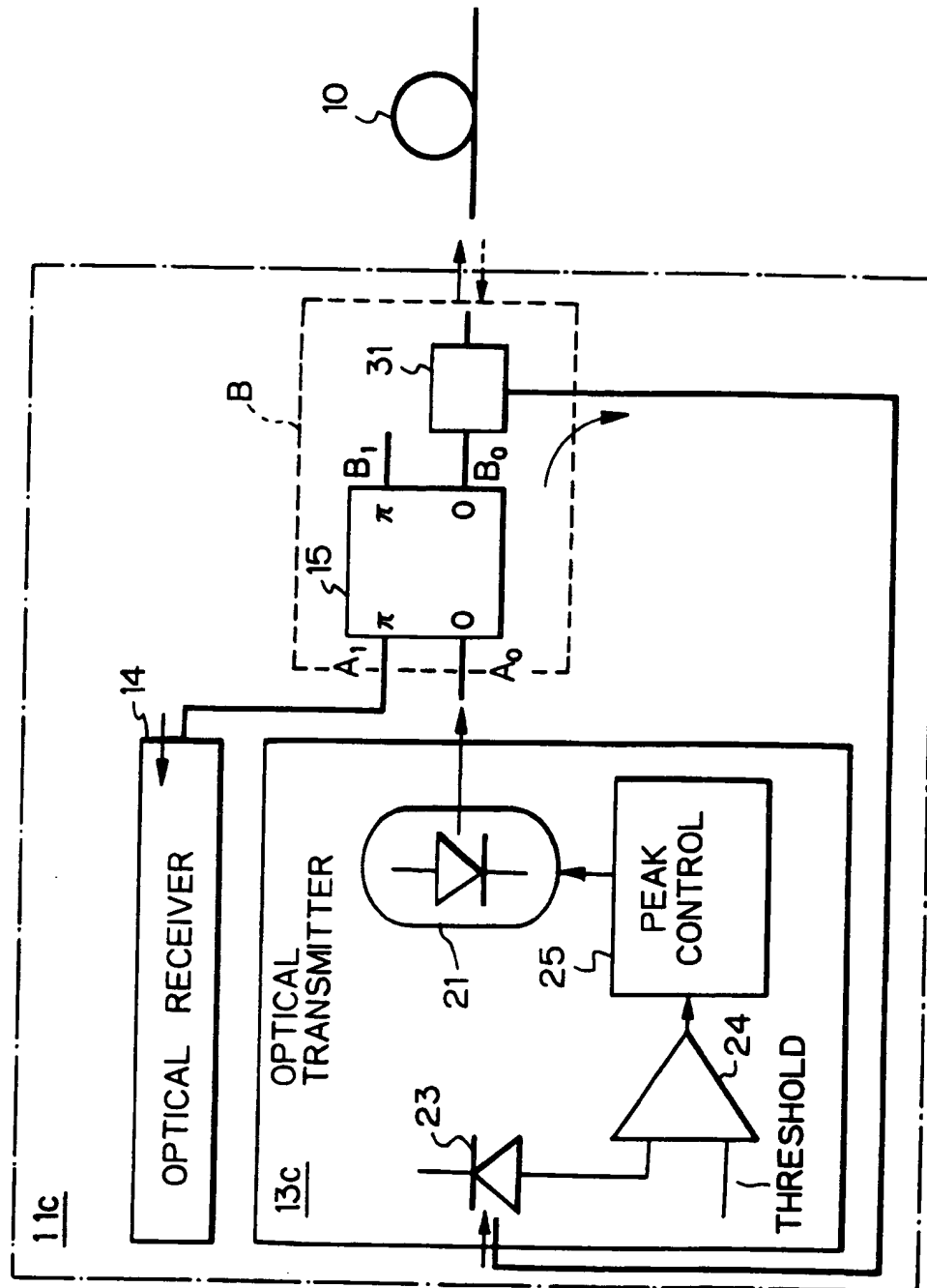


Fig. 4C

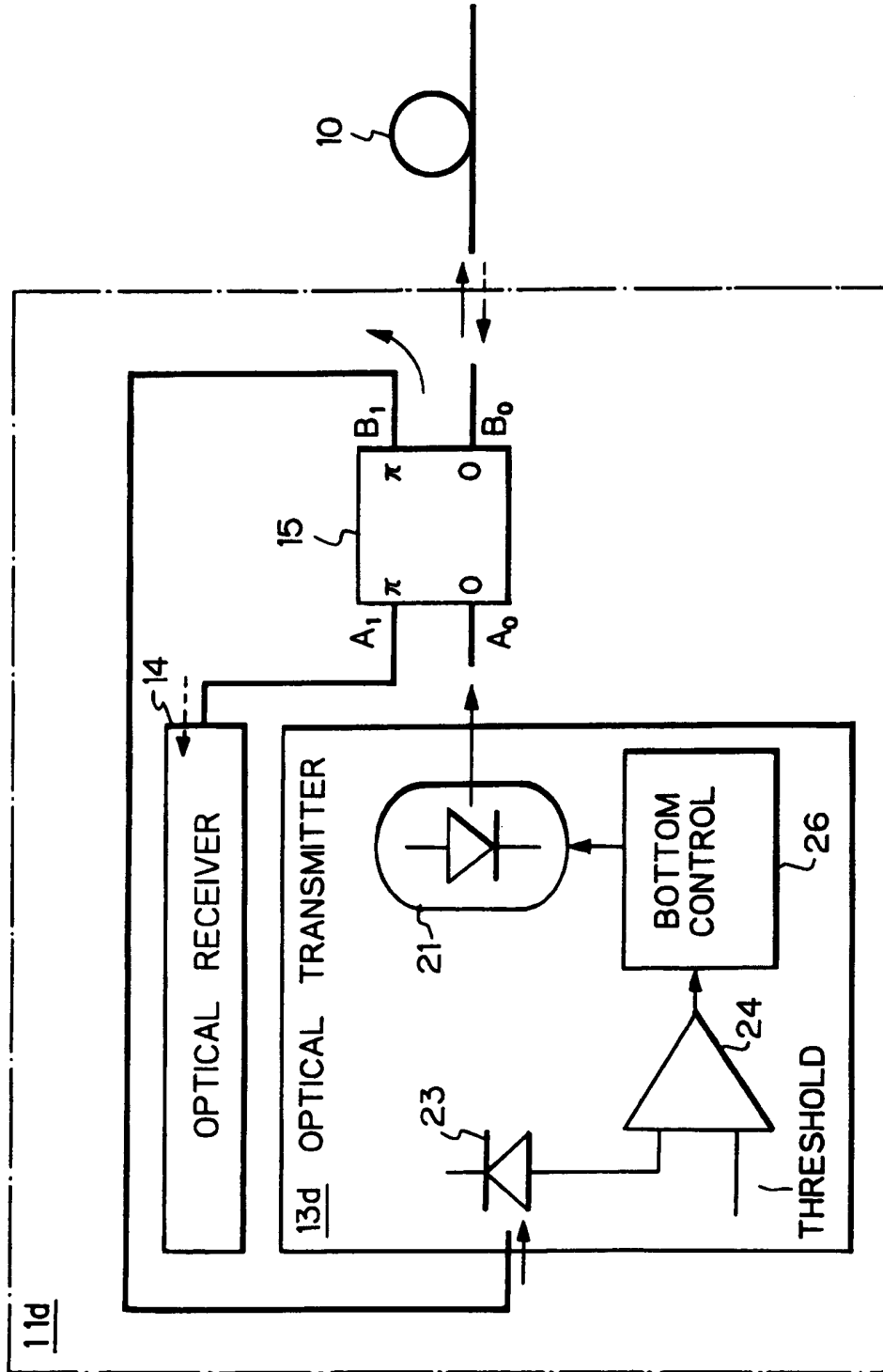




Fig. 5A

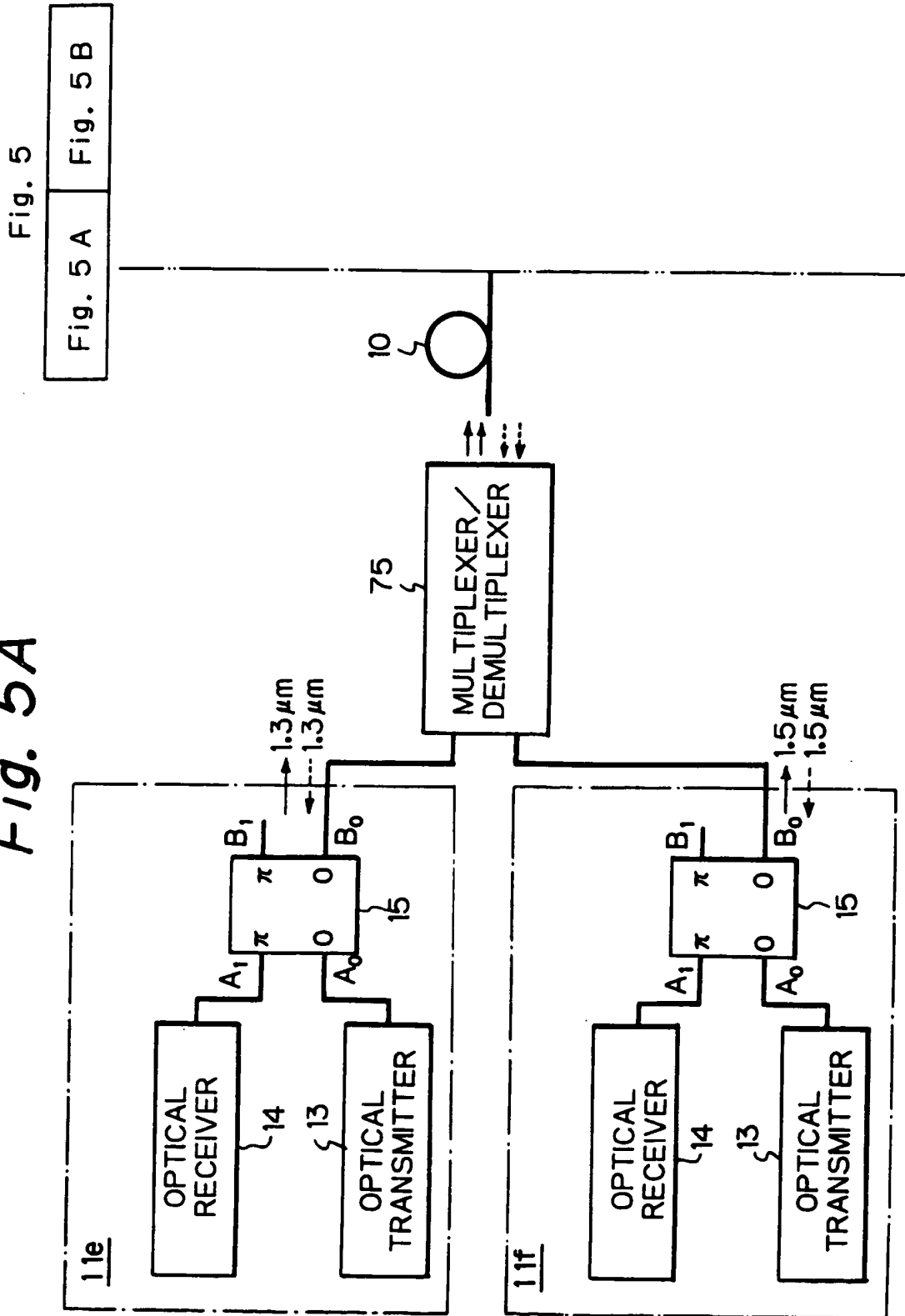


Fig. 5B

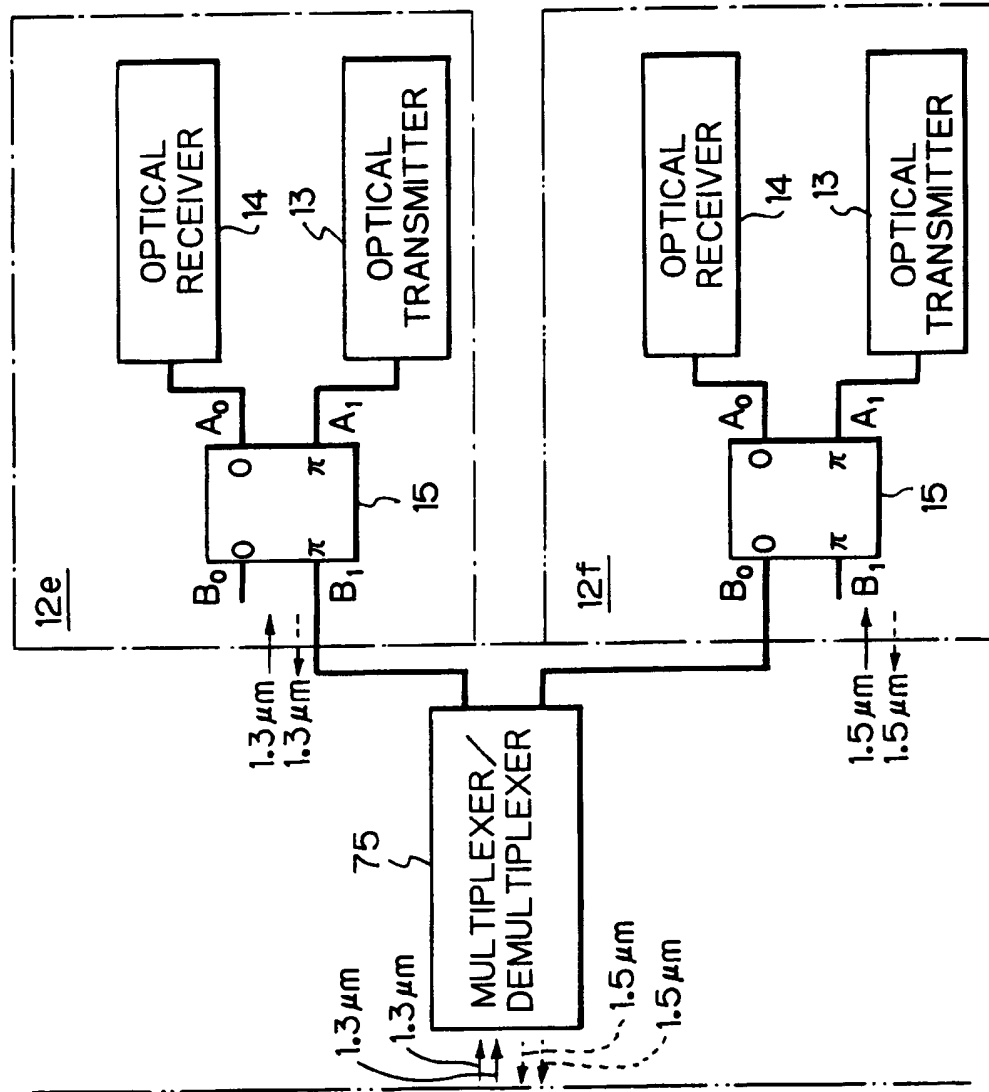


Fig. 6A

Fig. 6

Fig. 6 A Fig. 6 B

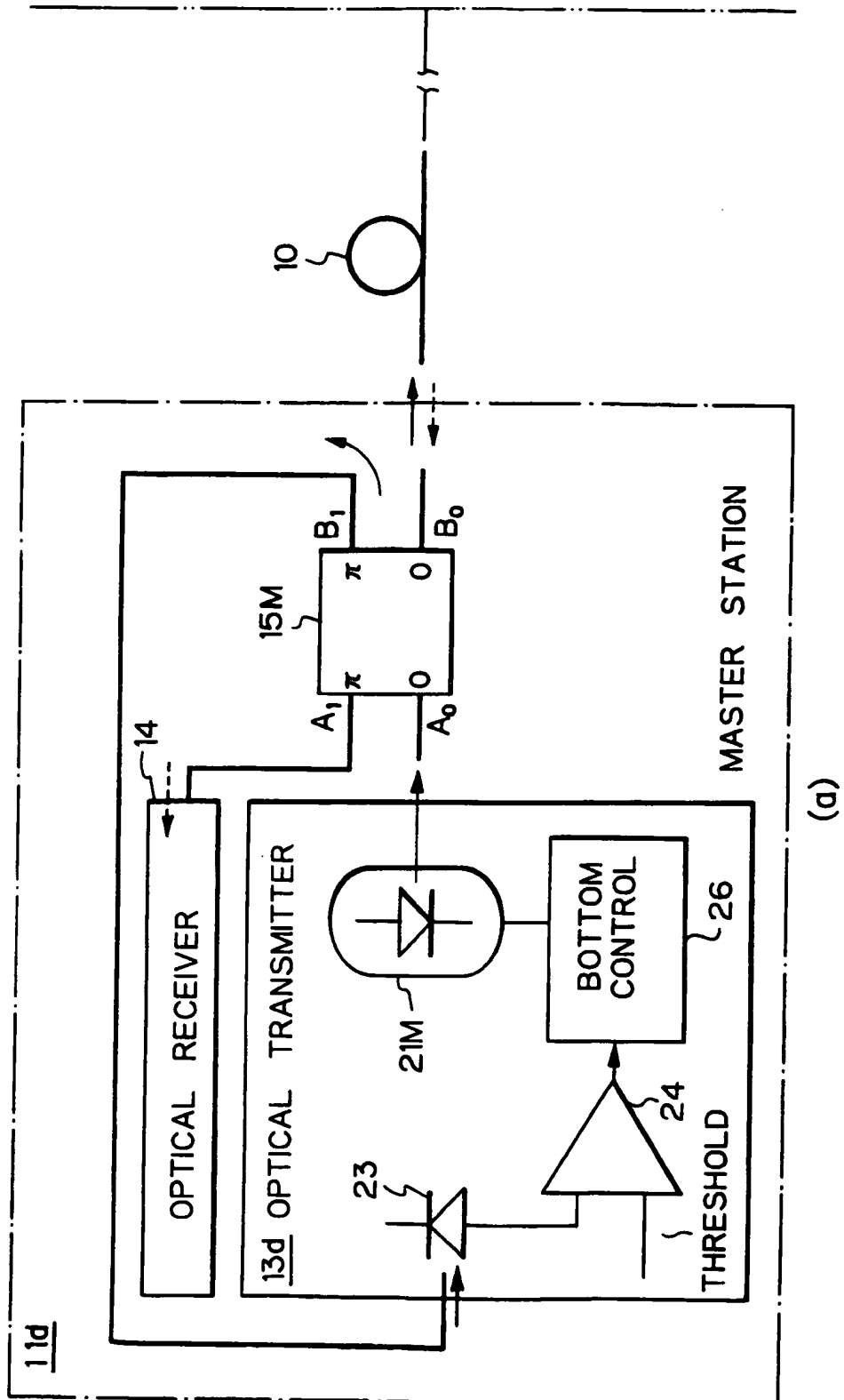
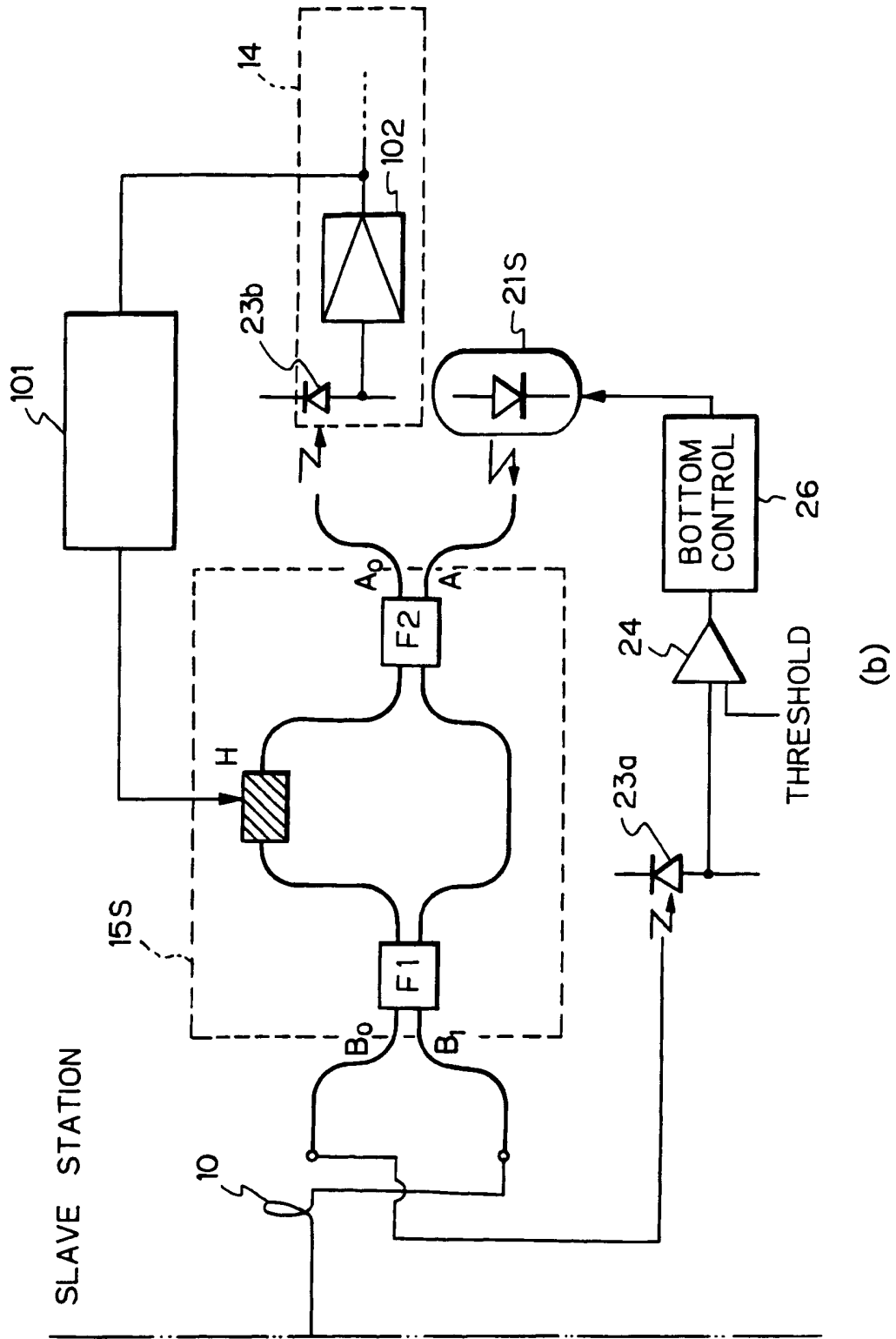


Fig. 6B

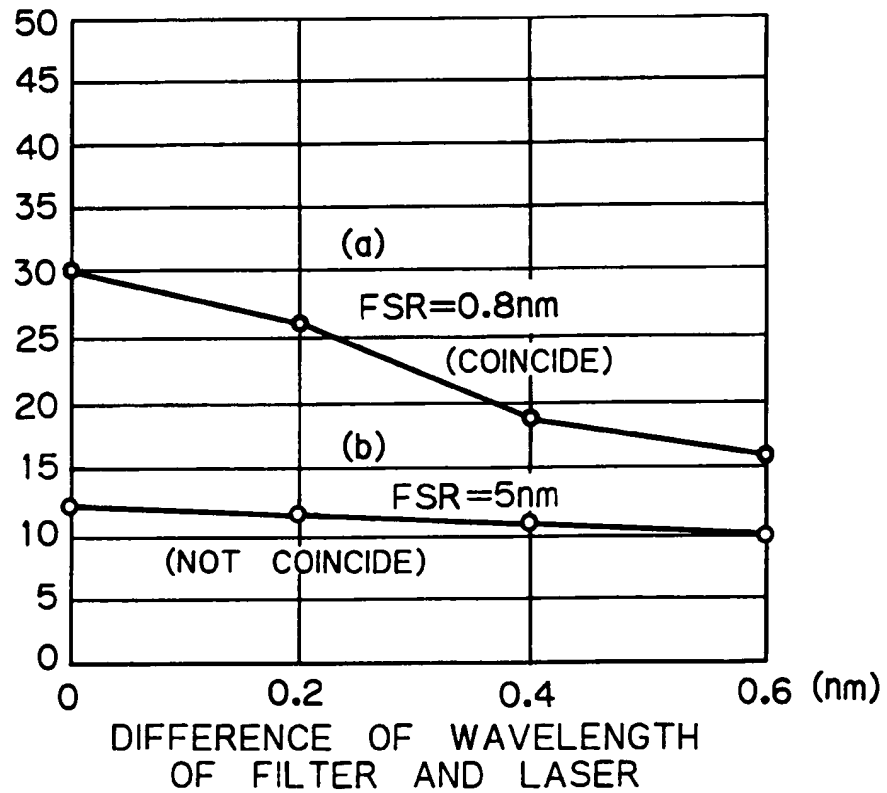


(b)

*Fig. 7*

ATTENUATION

(dB)



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